

# Synthesis and magnetic properties of $\text{Fe}_5\text{C}_2$ by reaction of iron oxide and carbon monoxide

S.-I. HIRANO, S. TAJIMA

*Department of Applied Chemistry, Faculty of Engineering, Nagoya University, Furo-cho, Chikusa-ku, Nagoya 464, Japan*

The formation behaviour and magnetic properties of  $\text{Fe}_5\text{C}_2$  were investigated. Iron oxides, as starting material, were carburized with carbon monoxide gas by heat treatment.  $\text{Fe}_5\text{C}_2$  was formed as a single phase in the reaction temperature range 350 to 375°C. The amount of carbon monoxide gas was controlled by mixing with nitrogen gas to prevent free carbon deposition by the disproportionation of carbon monoxide. Synthesized  $\text{Fe}_5\text{C}_2$  particles were identified as a single phase by XRD and the weight change measurement of reactants. The saturation magnetization of  $\text{Fe}_5\text{C}_2$  was about 100 e.m.u.  $\text{g}^{-1}$ , regardless of the reaction temperature. The coercive force decreased from 800 to 400 Oe with increasing reaction temperature.

## 1. Introduction

Recently, magnetic particles with high saturation magnetization have been expected to be synthesized as high quality video and cassette tapes. At present, maghaematite ( $\gamma\text{-Fe}_2\text{O}_3$ ) is mainly used as a magnetic recording medium, because of the easy mass production of  $\gamma\text{-Fe}_2\text{O}_3$  with an appropriate value of the saturation magnetization and the coercive force. Oxide magnetic materials, however, have a relatively low saturation magnetization, below 90 e.m.u.  $\text{g}^{-1}$ .

Thus, metallic iron particles have attracted attention for use as a new magnetic recording medium, which has a very high saturation magnetization ( $\sim 200$  e.m.u.  $\text{g}^{-1}$ ). The inferior chemical stability of the metallic iron particles is known to be a serious disadvantage in use. The surface of the iron particles is gradually oxidized in air to form iron oxides of lower saturation magnetization for stabilization. The commercially available iron particles have a saturation magnetization of 130 to 150 e.m.u.  $\text{g}^{-1}$ . On the other hand, the coercive force of iron powder is very high value ( $> 1000$  Oe).

Iron nitrides such as  $\text{Fe}_4\text{N}$ ,  $\text{Fe}_{16}\text{N}$ , etc., also have higher saturation magnetization than  $\gamma\text{-Fe}_2\text{O}_3$  and higher chemical resistances than metallic iron particles, and are expected to be used for new magnetic recording materials [1, 2]. Among these nitrides,  $\text{Fe}_4\text{N}$  has a very high saturation magnetization ( $\sim 190$  e.m.u.  $\text{g}^{-1}$ ) [3]. There is a wide stable region of  $\text{Fe}_4\text{N}$  in the Fe-N system phase diagram [1], which enables synthesis of  $\text{Fe}_4\text{N}$  as a single phase from iron metal and ammonia gas [4, 5]. The coercive force of the  $\text{Fe}_4\text{N}$  formed is  $\sim 800$  Oe which is appropriate for utilization as a magnetic tape [4, 5]. However,  $\text{Fe}_4\text{N}$  also exhibits a low chemical stability causing a decrease in the high saturation magnetization ( $\sim 100$  e.m.u.  $\text{g}^{-1}$ ) due to surface oxidation [4, 5].

Some iron carbides are candidates for magnetic

materials, especially  $\text{Fe}_3\text{C}$ ,  $\text{Fe}_5\text{C}_2$  and  $\text{Fe}_7\text{C}_3$  [6-9]. These iron carbides have acceptably high saturation magnetization ( $\sim 130$  e.m.u.  $\text{g}^{-1}$ ) [10], although the value is lower than those of metallic iron and  $\text{Fe}_4\text{N}$ . They also have the great advantages of higher resistance to oxidation than metals and nitrides, and of suitable hardness. Therefore, iron carbides are expected to be promising as new magnetic recording media. However, it is difficult to synthesize a desired iron carbide as a single phase, because most iron carbides are metastable under 1 atm pressure [11]. Iron carbides prepared so far are also contaminated with metallic iron, iron oxides, free carbon and other iron carbides. Few papers have reported the formation behaviour and properties of iron carbides except for the saturation magnetization and the Curie points of  $\text{Fe}_3\text{C}$ ,  $\text{Fe}_5\text{C}_2$  and  $\text{Fe}_7\text{C}_3$  [9, 10, 12].

Among these carbides,  $\text{Fe}_5\text{C}_2$  has a relatively high saturation magnetization and is well known as the Hägg carbide [6]. However a study of the synthesis of pure  $\text{Fe}_5\text{C}_2$  is required. This work focuses on the formation behaviour and magnetic properties of pure  $\text{Fe}_5\text{C}_2$  for possible use as a magnetic recording medium.

## 2. Experimental procedure

$\alpha\text{-Fe}_2\text{O}_3$  and  $\text{Fe}_3\text{O}_4$  powders were used as starting iron sources. Table I shows the characteristics of the starting iron oxides. The particle size and shape of iron oxides were observed using a transmission electron microscope (TEM). The BET method was used to examine the specific surface area.  $\alpha\text{-Fe}_2\text{O}_3(1)$  listed in Table I was a chemical reagent.

$\alpha\text{-Fe}_2\text{O}_3(2)$  particles were prepared by the thermal decomposition of  $\alpha\text{-FeOOH}$  as follows:  $\text{Fe}(\text{NO}_3)_2 \cdot 9\text{H}_2\text{O}$  was dissolved in deionized water to the concentration of about  $0.1 \text{ mol l}^{-1}$ . A small excess of KOH aqueous solution was added to the aqueous solution and then stirred for 3 d to yield a yellow

TABLE I Specific surface area (BET method), particle size and particle shape of starting iron oxides

	Particle size ( $\mu\text{m}$ )	Surface area ( $\text{m}^2 \text{g}^{-1}$ )	Particle shape
$\alpha\text{-Fe}_2\text{O}_3(1)$	0.2–0.6	7.6	Granular
$\alpha\text{-Fe}_2\text{O}_3(2)$	$\sim 1$	117	Acicular
$\text{Fe}_3\text{O}_4$	$\sim 0.02$	120	Granular

precipitate ( $\alpha\text{-FeOOH}$ ).  $\alpha\text{-FeOOH}$  thus formed was filtered and dried by thermal decomposition at  $300^\circ\text{C}$  for 1 h in air.

$\text{Fe}_3\text{O}_4$  particles were prepared by dissolving  $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$  and  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  (molar ratio 1 : 2) in deionized water to a concentration of about  $0.1 \text{ mol l}^{-1}$ . A small excess of aqueous  $\text{NaOH}$  was added to the aqueous solution to yield a black precipitate ( $\text{Fe}_3\text{O}_4$ ). The precipitated  $\text{Fe}_3\text{O}_4$  was dried at  $100^\circ\text{C}$  for 1 d.

Fig. 1 shows the experimental apparatus used in this work. About 500 mg of the starting iron oxide particles were placed in an alumina boat and put in an electric furnace with a quartz inner tube. After the iron oxide particles were heated to a prescribed temperature in a flow of nitrogen gas, carbon monoxide gas was passed into the quartz tube. Nitrogen gas was used to dilute the carbon monoxide gas. After heat treatment, the specimens were cooled in the furnace in a flow of nitrogen gas. The weight change of the specimens was measured before and after the heat treatment under the following experimental conditions: reaction temperature 250 to  $600^\circ\text{C}$ ; holding time 1 to 4 h; carbon monoxide gas flow rate  $50 \text{ ml min}^{-1}$ ; nitrogen gas flow rate 0 to  $350 \text{ ml min}^{-1}$ . The weight change of the specimens was determined from the equation

$$\text{weight change (\%)} = \frac{\text{weight of treated specimen} - \text{weight of starting iron oxide}}{\text{weight of starting iron oxide}} \quad (1)$$

The crystalline phases of the products were identified by X-ray diffractometry (XRD). The intensity ratio of  $\text{Fe}_5\text{C}_2(510)$  and  $\text{Fe}_3\text{O}_4(311)$  X-ray profiles was measured to calculate the formation of  $\text{Fe}_5\text{C}_2$  in the specimens from the equation

$$\text{Fe}_5\text{C}_2 \text{ content (wt \%)} = \frac{I_{\text{Fe}_5\text{C}_2 510}}{I_{\text{Fe}_5\text{C}_2 510} + 0.33I_{\text{Fe}_3\text{O}_4 311}} \quad (2)$$

The magnetic properties of the products were measured by a vibrating sample magnetometer (VSM) at room temperature in a magnetic field up to 17.5 kOe.

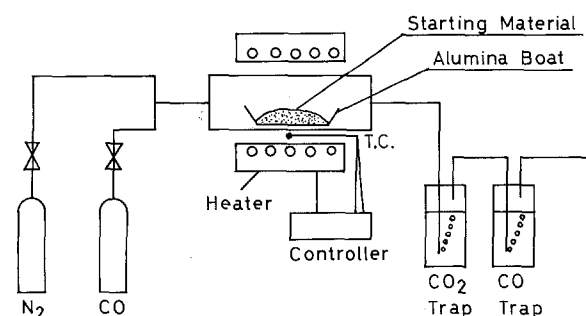


Figure 1 Experimental apparatus. TC = thermocouple.

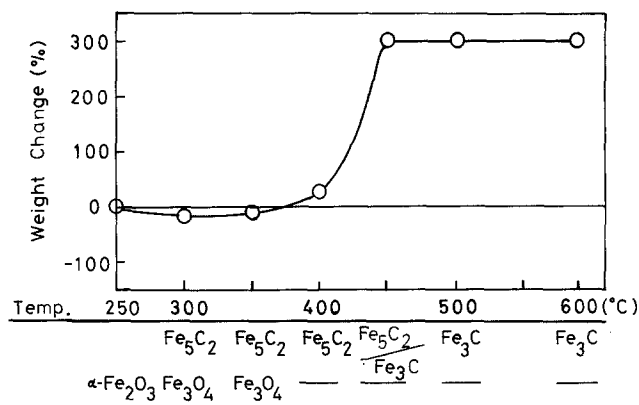


Figure 2 Effect of reaction temperature on phases formed and weight change of specimens; holding time 4 h, carbon monoxide gas flow rate  $50 \text{ ml min}^{-1}$ , starting iron oxide  $\alpha\text{-Fe}_2\text{O}_3$ . Weight gain: carbon formation by disproportionation of carbon monoxide gas. Weight loss: reduction from iron oxide to iron carbide.

### 3. Results and discussion

#### 3.1. Effect of reaction temperature on the phase formed and the weight change of specimens

Fig. 2 shows the dependence of the weight change of the specimens on the reaction temperature and of the crystalline phases on the reaction temperature. The experimental conditions were: reaction temperature 250 to  $600^\circ\text{C}$ ; holding time 4 h; carbon monoxide gas flow rate  $50 \text{ ml min}^{-1}$ ; starting iron oxide  $\alpha\text{-Fe}_2\text{O}_3$ .

Carburization did not occur on heating in carbon monoxide gas below  $250^\circ\text{C}$ . The desired carbide of  $\text{Fe}_5\text{C}_2$  was formed in the reaction temperature range 300 to  $450^\circ\text{C}$ .  $\text{Fe}_3\text{O}_4$  particles formed from  $\alpha\text{-Fe}_2\text{O}_3$

coexisted in the specimens at temperatures between 300 and  $350^\circ\text{C}$ , while  $\text{Fe}_3\text{C}$  formed in the reaction temperature range 450 to  $600^\circ\text{C}$ .  $\text{Fe}_5\text{C}_2$  was not formed above  $450^\circ\text{C}$ . No other iron compounds, except  $\text{Fe}_3\text{O}_4$ ,  $\text{Fe}_5\text{C}_2$  and  $\text{Fe}_3\text{C}$ , were detected by XRD under these conditions. These results indicate that  $\text{Fe}_5\text{C}_2$  does form at temperatures between 250 and  $450^\circ\text{C}$  and  $\text{Fe}_3\text{C}$  becomes the main product above  $450^\circ\text{C}$ . Hofer and Cohn [10] also reported that  $\text{Fe}_5\text{C}_2$  decomposed to  $\text{Fe}_3\text{C}$  and carbon above  $550^\circ\text{C}$ .

The total weight of the specimens decreases by about 20% if the reduction from  $\alpha\text{-Fe}_2\text{O}_3$  to iron carbide occurs. The weight change of the specimens was not observed at  $250^\circ\text{C}$ , because the starting iron oxide could not react to form the carbide. In the reaction temperature range 300 to  $350^\circ\text{C}$ , the weight change was less than 20%, because  $\text{Fe}_3\text{O}_4$  was co-precipitated with carbide by reduction with  $\alpha\text{-Fe}_2\text{O}_3$ . Free carbon was deposited in the specimens at temperatures from 400 to  $600^\circ\text{C}$  by the disproportionation of carbon monoxide gas to form carbon dioxide and free carbon. Above  $450^\circ\text{C}$ , a large amount of free carbon was deposited, which reflects the large weight change of the specimens to above 300%. The formation of free carbon and residual

$\text{Fe}_3\text{O}_4$  must be avoided in order to synthesize  $\text{Fe}_5\text{C}_2$  as a single phase.

The above results indicate that the reaction temperature of  $375^\circ\text{C}$  was suitable to synthesize  $\text{Fe}_5\text{C}_2$  particles as a single phase to avoid the deposition of free carbon. The formation behaviour of  $\text{Fe}_5\text{C}_2$  at this temperature was investigated in detail.

### 3.2. Effect of iron oxides on the formation of $\text{Fe}_5\text{C}_2$

Table II shows the effect of starting iron oxides on the reaction of the specimens and the phases formed at  $375^\circ\text{C}$  under the following experimental conditions: holding time 4 h; carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ ; nitrogen gas flow rate  $350\text{ ml min}^{-1}$ .

When  $\alpha\text{-Fe}_2\text{O}_3(1)$  was used as a starting iron oxide, the amount of  $\text{Fe}_5\text{C}_2$  formed was about 80 wt %. On the other hand, the amount of  $\text{Fe}_5\text{C}_2$  formed from  $\alpha\text{-Fe}_2\text{O}_3(2)$  and  $\text{Fe}_3\text{O}_4$  was 100 wt %. It was found that the particle size of the starting iron oxide strongly affected the formation of  $\text{Fe}_5\text{C}_2$ .  $\alpha\text{-Fe}_2\text{O}_3(1)$  particles have a smaller surface area than  $\alpha\text{-Fe}_2\text{O}_3(2)$  and  $\text{Fe}_3\text{O}_4$  (as seen in Table I). The result suggests that such a solid state reaction requires that the starting materials, have a small size and high surface area. Therefore, a longer holding time was required in order to carburate perfectly  $\alpha\text{-Fe}_2\text{O}_3(1)$  under these conditions. When  $\alpha\text{-Fe}_2\text{O}_3$  was used as starting iron oxide, no iron compounds except  $\text{Fe}_3\text{O}_4$  and  $\text{Fe}_5\text{C}_2$  were detected in the treated specimens. These results reveal that  $\alpha\text{-Fe}_2\text{O}_3$  was reduced to  $\text{Fe}_3\text{O}_4$ , which was subsequently carburated to  $\text{Fe}_5\text{C}_2$  under the above conditions.

As shown in Table II, the weight change of  $\alpha\text{-Fe}_2\text{O}_3(2)$  on carburization was larger than that of  $\text{Fe}_3\text{O}_4$ . Only  $\text{Fe}_5\text{C}_2$  was detected as a crystalline phase in the specimens formed from both the starting iron oxides. The result indicates that the amount of free carbon deposited with  $\text{Fe}_5\text{C}_2$  formed from  $\alpha\text{-Fe}_2\text{O}_3(2)$  was larger than that from  $\text{Fe}_3\text{O}_4$ .

The particle size of  $\text{Fe}_5\text{C}_2$  formed from  $\alpha\text{-Fe}_2\text{O}_3(1)$  was about  $1\ \mu\text{m}$  and larger than that of the starting  $\alpha\text{-Fe}_2\text{O}_3(1)$ . The particle size of  $\text{Fe}_5\text{C}_2$  formed from  $\alpha\text{-Fe}_2\text{O}_3(2)$  was about  $0.1\ \mu\text{m}$ . The acicular shape of  $\alpha\text{-Fe}_2\text{O}_3(2)$  particles as starting iron oxide could not be maintained in the  $\text{Fe}_5\text{C}_2$  particles formed. The particle size of  $\text{Fe}_5\text{C}_2$  formed from  $\text{Fe}_3\text{O}_4$  was about  $0.1\ \mu\text{m}$  and larger than that of original  $\text{Fe}_3\text{O}_4$  particles.

From the viewpoint of the reactivity and particle size of the  $\text{Fe}_5\text{C}_2$  formed,  $\text{Fe}_3\text{O}_4$  particles were selected as the most appropriate starting iron oxide for the preparation of  $\text{Fe}_5\text{C}_2$  particles.

TABLE II Effect of starting iron oxides on formation behaviour of  $\text{Fe}_5\text{C}_2$  at  $375^\circ\text{C}$  for 4 h; carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ , nitrogen gas flow rate  $350\text{ ml min}^{-1}$

Starting iron oxide	Weight change (%)	$\text{Fe}_5\text{C}_2$ content (wt %)
$\alpha\text{-Fe}_2\text{O}_3(1)$	-14	83
$\alpha\text{-Fe}_2\text{O}_3(2)$	-9	100
$\text{Fe}_3\text{O}_4$	-20	100

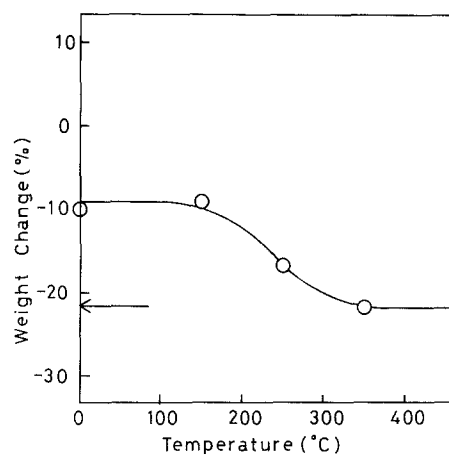


Figure 3 Relationship between weight change of specimens and nitrogen gas flow rate; reaction temperature  $375^\circ\text{C}$ , holding time 4 h, carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ , starting iron oxide  $\text{Fe}_3\text{O}_4$ .

### 3.3. Effect of nitrogen flow rate and holding time on the reaction to form $\text{Fe}_5\text{C}_2$

In order to decrease the amount of free carbon deposited by the disproportionation of carbon monoxide gas, the gas had to be diluted with nitrogen gas. At temperatures around  $400^\circ\text{C}$ , iron oxide does not react with nitrogen to form nitrides. Fig. 3 shows the relationship between the weight change of the specimens and the nitrogen gas flow rate under the following experimental conditions: treatment temperature  $375^\circ\text{C}$ ; holding time 4 h; carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ ; starting iron oxide  $\text{Fe}_3\text{O}_4$ .

The total weight change on the formation of  $\text{Fe}_5\text{C}_2$  from  $\text{Fe}_3\text{O}_4$  can be theoretically calculated to be about  $-20\%$ , which is shown by an arrow in Fig. 3. The weight change of the specimens was close to  $-20\text{ wt %}$  with increasing nitrogen gas flow rate. When the nitrogen gas flow rate was adjusted to  $350\text{ ml min}^{-1}$ , the weight change reached about  $-20\text{ wt %}$ , in which only  $\text{Fe}_5\text{C}_2$  phase formed in the specimens. These results indicate that the amount of deposited free carbon decreased with increasing nitrogen gas flow rate and  $\text{Fe}_5\text{C}_2$  formed as a single phase under these conditions. A representative X-ray diffraction profile of the  $\text{Fe}_5\text{C}_2$  formed is shown in Fig. 4. The intensity and the lattice parameters agreed with those of  $\text{Fe}_5\text{C}_2$  [13].

Fig. 5 shows the relationship between the content of  $\text{Fe}_5\text{C}_2$  formed and the holding time. The experimental conditions were controlled as follows, according to the above results, to avoid the deposition of free carbon: reaction temperature  $375^\circ\text{C}$ ; carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ ; nitrogen gas flow rate  $350\text{ ml min}^{-1}$ ; starting iron oxide  $\text{Fe}_3\text{O}_4$ .

The content of  $\text{Fe}_5\text{C}_2$  formed increased with increasing holding time and reached 100 wt % when the holding time was longer than 2 h. No crystalline phases except  $\text{Fe}_5\text{C}_2$  and  $\text{Fe}_3\text{O}_4$  were detected regardless of the change in holding time under these conditions.

### 3.4. Effect of reaction temperature on magnetic properties of $\text{Fe}_5\text{C}_2$ particles formed

The conditions necessary for the preparation of  $\text{Fe}_5\text{C}_2$

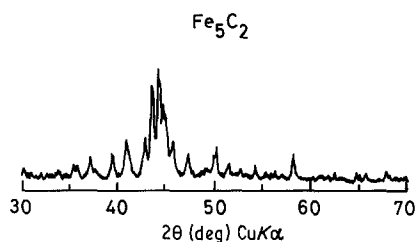


Figure 4 Representative X-ray diffraction profile of  $\text{Fe}_5\text{C}_2$  formed as a single phase from  $\text{Fe}_3\text{O}_4$  at  $375^\circ\text{C}$  for 4 h; carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ , nitrogen gas flow rate  $350\text{ ml min}^{-1}$ .

particles as a single phase were determined to be as follows: reaction temperature  $350$  to  $375^\circ\text{C}$ ; holding time 2 to 4 h; carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ ; nitrogen gas flow rate  $350\text{ ml min}^{-1}$ ; starting iron oxide  $\text{Fe}_3\text{O}_4$ . The size of the granular  $\text{Fe}_5\text{C}_2$  particles formed under these conditions was about  $0.1\ \mu\text{m}$ . Fig. 6 shows the relationship between the magnetic properties of  $\text{Fe}_5\text{C}_2$  particles formed and the reaction temperature. The saturation magnetization of the products was found to be about  $100\text{ e.m.u. g}^{-1}$  regardless of the reaction temperature. However,  $\text{Fe}_5\text{C}_2$  particles were contaminated with 10 wt % free carbon particles which were deposited by the disproportionation of carbon monoxide gas at  $400^\circ\text{C}$ . Thus, the saturation magnetization of pure  $\text{Fe}_5\text{C}_2$  can be suggested by taking the coexistence of 10 wt % free carbon into account according to the following equation

$$\begin{aligned} \text{corrected } \sigma_s (\text{e.m.u. g}^{-1}) &= 1.1 \\ &\times \text{measured } \sigma_s (\text{e.m.u. g}^{-1}) \end{aligned}$$

The value is corrected to about  $100\text{ e.m.u. g}^{-1}$ . Hofer and Cohn [10] reported that the saturation magnetization of  $\text{Fe}_5\text{C}_2$  was about  $130\text{ e.m.u. g}^{-1}$ . The difference in the saturation magnetization may be attributable to the difference in the state of the crystal perfection of  $\text{Fe}_5\text{C}_2$ .

The coercive force of  $\text{Fe}_5\text{C}_2$  particles formed decreased from 800 to 400 Oe with increase in the reaction temperature, because the particle size of the

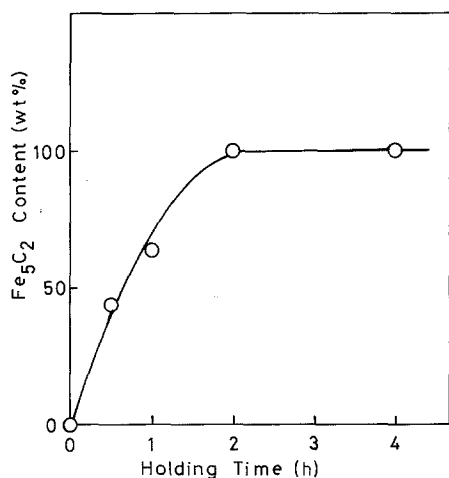


Figure 5 Relationship between the amount of  $\text{Fe}_5\text{C}_2$  formed in treated specimens and holding time; reaction temperature  $375^\circ\text{C}$ , carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ , nitrogen gas flow rate  $350\text{ ml min}^{-1}$ , starting iron oxide  $\text{Fe}_3\text{O}_4$ .

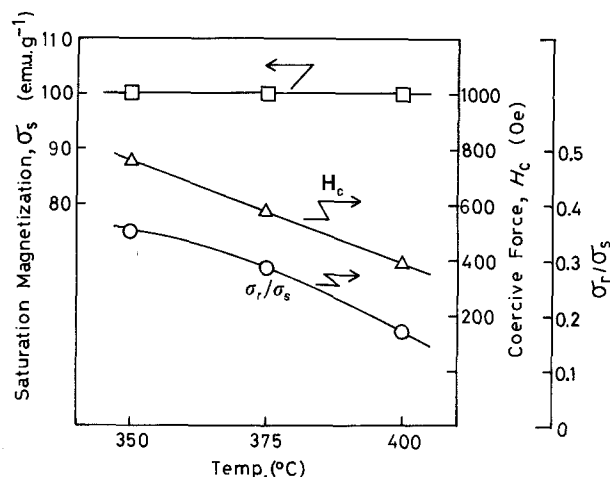


Figure 6 Effect of reaction temperature on magnetic properties of  $\text{Fe}_5\text{C}_2$  formed from  $\text{Fe}_3\text{O}_4$ ; holding time 4 h, carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ , nitrogen gas flow rate  $350\text{ ml min}^{-1}$ .

$\text{Fe}_5\text{C}_2$  particles formed increased with increasing reaction temperature and reached the multi-magnetic-domain size. The coercive force of the commercially available magnetic recording powder is controlled to 300 to 1000 Oe, therefore this coercive force of 400 to 800 Oe may be an appropriate value for use as a magnetic recording medium. A representative hysteresis loop of  $\text{Fe}_5\text{C}_2$  particles formed as a single phase is shown in Fig. 7.

The ratio of the residual magnetization to the saturation magnetization ( $=\sigma_r/\sigma_s$ ) also decreased from 0.35 to 0.17 with increase in the reaction temperature, the same behaviour as the decrease in the coercive force. The  $\sigma_r/\sigma_s$  ratio of the commercially available magnetic recording powders is normally  $>0.5$ . The value of  $\sigma_r/\sigma_s$  ratio must be improved in  $\text{Fe}_5\text{C}_2$  particles formed in this work by adjustment of the crystallinity and particle shape.

There are uncertainties in the magnetocrystalline anisotropy constant, the magnetostrictive constant and the single domain size of  $\text{Fe}_5\text{C}_2$ , which must be determined for pure  $\text{Fe}_5\text{C}_2$  particles. The coercive force and  $\sigma_r/\sigma_s$  ratio of  $\text{Fe}_5\text{C}_2$  formed in this work can be improved if well-crystallized fine and acicular particles of  $\text{Fe}_5\text{C}_2$  can be formed by control of the reaction conditions.

The saturation magnetization and the coercive force of  $\text{Fe}_5\text{C}_2$  particles formed did not change after the

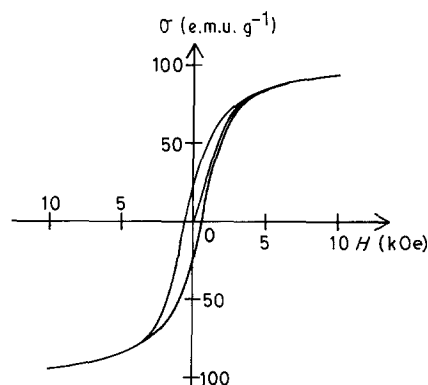


Figure 7 Representative hysteresis loop of  $\text{Fe}_5\text{C}_2$  formed as a single phase from  $\text{Fe}_3\text{O}_4$  at  $375^\circ\text{C}$  for 4 h; carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ , nitrogen gas flow rate  $350\text{ ml min}^{-1}$ .

particles formed were stored in ambient air for 1 month. This result reveals that the  $\text{Fe}_5\text{C}_2$  particles formed are chemically stable in an ambient atmosphere.

#### 4. Conclusions

Iron oxides and carbon monoxide gas were used as starting materials to synthesize  $\text{Fe}_5\text{C}_2$  particles. The formation behaviour of iron carbides and the magnetic properties of the iron carbides formed were investigated. The following results were obtained.

1. When the reaction temperature was  $250^\circ\text{C}$  or below, iron carbides did not form on carburization with carbon monoxide. In the reaction temperature range  $300$  to  $400^\circ\text{C}$ ,  $\text{Fe}_5\text{C}_2$  was formed as a major phase.  $\text{Fe}_3\text{C}$  was predominantly formed above  $450^\circ\text{C}$ .

2.  $\text{Fe}_5\text{C}_2$  can be synthesized as a single phase under the following conditions: reaction temperature  $350$  to  $375^\circ\text{C}$ ; holding time  $2$  to  $4$  h; starting iron oxide  $\text{Fe}_3\text{O}_4$ ; nitrogen gas flow rate  $350\text{ ml min}^{-1}$ ; carbon monoxide gas flow rate  $50\text{ ml min}^{-1}$ .

3. The saturation magnetization of  $\text{Fe}_5\text{C}_2$  particles was about  $100\text{ e.m.u. g}^{-1}$  regardless of the reaction temperature. The coercive force of  $\text{Fe}_5\text{C}_2$  decreased with increasing reaction temperature from  $800$  to  $400\text{ Oe}$ , depending upon the increase in particle size.

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